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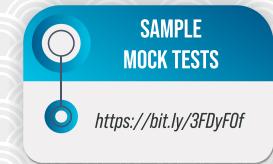
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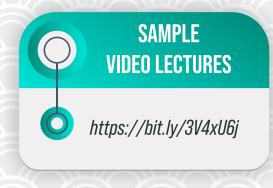


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IC ENGINE

Chapter 1: AIR STANDARD CYCLES

$$Clearance \ ratio(C) = \frac{v_c}{v_s}$$

 v_c = Clearance volume

 v_S = Swept volume

 $\text{Compression ratio (r)} = \frac{v_c + v_s}{v_c}$

 $=\frac{\pi}{4} d^2L$

d = Bore di<mark>a</mark>meter

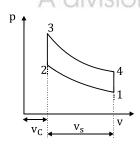
L = Stroke Length

Compression ratio (r) = $\frac{v_c + v_s}{v_c}$



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1. Otto Cycle (S.I Engine)



$$\eta_{otto} = 1 - \left(\frac{1}{r}\right)^{\gamma - 1}$$

$$r = \frac{v_1}{v_2} = \frac{v_4}{v_3}$$

$$\frac{T_2}{T_1} = \frac{T_3}{T_4} = \left(\frac{v_4}{v_3}\right)^{\gamma - 1}$$

Note: η_{otto} for max work done

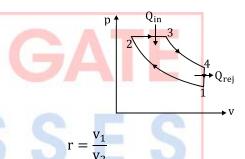
$$(\eta_o)_{max} = 1 - \sqrt{\frac{T_1}{T_3}}$$

Mean Effective pressure (MEP):

$$P_{MEP} = \frac{(WD)_{net}}{v_{swept}}$$

 r_{otto} varies between 6 to 12

2. Diesel Cycle (CI Engine)



$$r_e = Expansion ratio = \frac{v_4}{v_3}$$

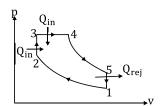
 $\rho(\text{cutoff ratio}) = \frac{v_3}{v_2}$

$$r_{\rm e} = \frac{r}{\rho}$$

$$\eta_{\text{diesel}} = 1 - \left(\frac{1}{r}\right)^{\gamma - 1} \left(\frac{\rho^{\gamma} - 1}{\gamma(\rho - 1)}\right)$$

 r_{diesel} varies between 16 to 22

3. **Dual Cycle:**



 η_{dual}

$$= 1$$

$$-\left(\frac{1}{r}\right)^{\gamma-1}\left(\frac{\alpha\;\rho^{\gamma}-1}{\gamma(\rho-1)\alpha+(\alpha-1)}\right)$$

pressure ratio $= \alpha = \frac{p_3}{p_2}$

Observation:

If
$$\alpha = 1$$
, $(p_3 = p_2) \rightarrow \text{Diesel cycle}$

If
$$\alpha = 1$$
, $\rho = 1 \rightarrow Otto$ cycle

r_{dual} varies between 12 to 16

Comparison of Otto, Diesel and Dual Cycle:

1. For same r and heat addition.

 $\eta_{\rm otto} > \eta_{\rm dual} > \eta_{\rm diesel}$

2. For same r and Q_{rejection}

 $\eta_{\rm otto} > \eta_{\rm dual} > \eta_{\rm diesel}$

3. For same peak pressure, peak temperature and $Q_{rejection}$

 $\eta_{diesel} > \eta_{dual} > \eta_{otto}$

4. For same peak pressure and heat input.

 $\eta_{diesel} > \eta_{dual} > \eta_{otto}$

5. For same peak pressure and work output.

 $\eta_{diesel} > \eta_{dual} > \eta_{otto}$

Engine Performance Parameters:

1. Heat added per second.

 $\frac{\text{HA}}{\text{sec}} = \dot{m}_{\text{fuel}} \times (\text{Calorific value})_{\text{fuel}}$

2. Indicated Power (IP):

Power available at piston due to the expansion of A/F mixture.

 $IP = \int pdv = Area of indicator$ diagram

3. Brake Power (BP):

Power available at the end of engine shaft.

$$BP = T_b \omega$$

 $T_b = Brake torque (N-m)$

$$\omega = \frac{2\pi N}{60} \; (\text{sec}^{-1})$$

4. Friction power (FP):

IP - BP



Indicated thermal efficiency

6

$$\eta_{\text{Thermal}} = \frac{\text{BP}}{\dot{m}_{\text{f}}(\text{CV})}$$

Brake Thermal efficiency

7.

$$\eta_{mechanical} = \frac{BP}{IP} = \frac{\eta_{Bth}}{\eta_{Ith}}$$

8. Relative efficiency:

$$\begin{split} \eta_{rel} &= \frac{Actual\ thermal\ efficeincy}{Air\ standard\ efficiency} \\ \eta_{rel} &= \frac{\eta_{Ith}\ or\ \eta_{Bth}}{\eta_{air\ standard}} \end{split}$$

9. Suction Flow Rate: $(\dot{\mathbf{v}}_s)$

 $\dot{v}_s = \frac{\pi}{4} D^2 L \times N \times K \quad (m^3/\text{sec})$



$$N = \frac{n}{2}$$
 for 4 stoke engine

N = n for 2 stoke engine

K = No. of cylinder

n = Speed of engine (in rps)

10. Mean Effective pressure:

Brake mean effective pressure

$$b_{mep} = \frac{BP}{\dot{v}_s}$$

Indicated mean effective pressure

$$i_{mep} = \frac{IP}{\dot{v}_s}$$

11. Specific Fuel consumption

Indicated specific fuel consumption.

$$i_{sfc} = \frac{\dot{m}_{fuel}}{IP}$$

Brake specific fuel consumption.

$$b_{sfc} = \frac{\dot{m}_{fuel}}{BP}$$

12. Average Piston Speed:

 $V_{piston} = 2 \times Stroke length$

$$\times \frac{N_{\rm rpm}}{60}$$

13.

$$\eta_{\text{vol}} = \frac{\dot{m}_{\nu_{\text{entry}}}}{\frac{\pi}{4} D^2 L \times N \times K}$$

Chapter 2: MORSE KEY TEST

4B = Brake Power when all the engines are firing.

$$3B = \frac{3B_1 + 3B_2 + 3B_3 + 3B_4}{4}$$

= Arithematic mean of engines firing when one of the engine is stopped one by one.

$$I = 4B - 3B$$

4I = 4(4B - 3B) Indicated power of engine

$$\eta_{mech} = \frac{4B}{4I}$$

Motoring Test:

- Used to find friction power of engine.
- rpm of running engine are noted.
- Motor is attached to engine shaft and made to run at same rpm. The
 power input to motor is friction power.

Chapter 3: COMBUSTION

Perfect Combustion

$$C_x H_y + z \left(O_2 + \frac{79}{21} N_2\right)$$

$$\rightarrow xCO_2 + \frac{y}{2} H_2O$$

$$+ z \left(\frac{79}{21}\right) N_2$$

$$Z = x + \frac{y}{4}$$

Stoichiometric AFR

⇒ No fuel in excess No air in excess { This ratio of AFM is stiochiometric AFR



Equivalency Ratio (φ):

$$\varphi = \frac{(\text{FAR})_{actual}}{(\text{FAR})_{stoichiometric}} = \frac{(\dot{m}_f)_{actual}}{(\dot{m}_f)_{ideal}}$$

If $\phi < 1 \Rightarrow$ Less temperature, less

Power, less knocking (in petrol).

If $1 \le \varphi < 1.4 \Rightarrow$ High temperature, high Power, high knocking (in petrol).

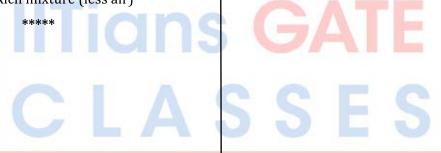
If $\phi > 1.4 \Rightarrow$ Same effect as $\phi < 1$.

Generally:

If $\phi = 1 \Rightarrow$ Chemically correct mixture

If $\phi < 1 \Rightarrow$ Lean mixture (Excess air)

IF $\phi > 1 \Rightarrow$ Rich mixture (less air)



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